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#### **Research Article**

# Structure based Virtual Screening of Rivastigmine Derivatives as Cholinesterase Inhibitors

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#### ABSTRACT

The interaction of large protein molecules with small drug molecules is studied through *in-silico* studies. The molecular docking and other important pharmacokinetic (ADMET) properties of the compounds were carried out with rivastigmine and its derivatives against protein bovine serum albumin (PDB: 4F5S) to describe their better protein-ligand interactions and binding affinities. Rivastigmine is a promising drug that is used to treat Alzheimer's disease. But due to the increased drug resistance property, its use becomes less effective. Hence, better drugs with higher potency are needed against this Alzheimer's disease. In order to design a more potent drug computationally, we have taken here 52 derivatives of rivastigmine and were docked against protein bovine serum albumin. Besides, quantum chemical parameters like HOMO-LUMO band gap energy and other important pharmacological analysis like ADMET studies were also carried out to predict better drug candidature. Molecular dynamics simulation and MMPBSA binding free energy calculations were also validated. From this computational study, 14 designed compounds were found to have better potency against Alzheimer's disease.

#### Introduction

Nowadays, the discovery of new drugs for any disease and replacing old ones is a challenging task. Rivastigmine in Fig. 1 is a cholinergic drug and the use of cholinesterase inhibitors were began in 1997. Besides, various cholinergic drugs like rivastigmine, donepezil, and galantamine were used to treat Alzheimer's disease. Acetylcholine inhibitors also block acetylcholine esterase (AChE) which results in controlling Alzheimer disease. In 2014, 5.3 million Americans suffered from Alzheimer disease. Acetylcholinesterase is an enzyme that hydrolyzes acetylcholine. Rivastigmine patch is a transdermal treatment and was previously practiced for dementia of Alzheimer disease in the United States.

Alzheimer and Parkinson disease both damage the human brain. It can cause death of many cells in the human brain. As a result of this disease, the effectiveness of human vision is also greatly reduced. Although the human memory

is fine at the beginning of the disease, gradually, the memory decreases a lot; changes in human behavior can be noticed. Alzheimer's disease causes behavioral changes in people and is treated with rivastigmine. Rivastigmine intake for a long time results in changes of the patient's behavior and mental state. [4] From 2000-2014, the death rate from Alzheimer's disease was increased by 89%. [3] The problem of this disease has increased with age. This disease's incidence doubles every 5 years when the patient is 65 years old. [5] The incidence of Alzheimer's disease is higher after 65 years. [6] Alzheimer's disease is a brain disease and rivastigmine improves brain function by enhancing human memory.<sup>[7]</sup> Once this disease starts, it gradually progresses and shows brain results in difficulty for the human body. People with this disease have higher difficulty for coordinating their various organs. Gradually it becomes difficult for people to speak and so people become nonsense.

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In this study, various derivatives of rivastigmine were designed and docked against protein bovine serum albumin (PDB: 4F5S). Through study, we would like to develop more advanced and highly effective drug compounds compared to rivastigmine to treat Alzheimer's disease. Different data have been taken by changing the functional group in different positions of the rivastigmine compound. Here, we have designed 52 new compounds followed by various useful analyses such as density functional theory (DFT), ADMET, molecular docking, and molecular dynamics simulation and find out 14 best-designed derivatives of rivastigmine against Alzheimer disease.

# MATERIALS AND METHODS

#### **Protein Preparation**

The three-dimensional X-ray crystal structure of the protein bovine serum albumin was retrieved from the protein data bank (PDB ID: 4F5S). Other chemical compounds were removed from the protein bovine serum albumin crystal structure before docking using Molegro Molecular Viewer (MMV)2.5.0 programme (CLC Bio, Qiagen Inc.).

### **Ligand Preparation**

All derivative ligand compounds along with the standard rivastigmine were drawn using ChemSketch Tool (ACD/Structure Elucidator, version 2018.1). The selected compounds having different substituents were shown in Table 1. Preparation of ligands includes adding all explicit hydrogens, 2D to 3D structure conversion. The molecules were optimized using DFT.<sup>[8,9]</sup>

# **Density Functional Theory Study**

Gaussian 09W<sup>[10]</sup> suite of software was used to minimize the energy search. Complete geometry optimization was done using DFT model restricted Becke's three parameters exchange potential and Lee-Yang-Parr correlation functional (RB3LYP) method and 6-31G(d,p) basis set.<sup>[11,12]</sup> These best compounds with their optimized structures are shown in Fig. 2. Highest occupied molecular orbital (HOMO), lowest unoccupied molecular orbital (LUMO), energy gap, total minimum energy and dipole moment were calculated and shown in Table 2.

#### **ADME and Toxicity Parameters**

PreADMET (http://preadmet.bmdrc.org/) server was used to test drug-likeness properties and ADME profiles (Absorption, Distribution, Metabolism, and Excretion) for all derived compounds. Molinspiration (http://www.molinspiration.com) and OSIRIS property explorer (http://www.organic-chemistry.org/prog/peo/) were also used to calculate various pharmacological parameters such as octanol-water partition coefficient (logP), solubility, topological polar surface area (TPSA), molecular weight (MW), drug-likeness, drug-score and number of violation

Fig. 1: Chemical structures of rivastigmine drug.

to Lipinski's rule. The overall toxicity for most active derivative compounds was predicted by OSIRIS program as it indicates fragment based properties responsible for mutagenic, tumorigenic, irritant, and reproductive effect.

# **Molecular Docking Method**

The docking protocol Autodockvina (ADT)[13] was used to predict the binding mode of rivastigmine and its derivatives into the binding site of protein bovine serum albumin (PDB ID: 4F5S). The receptor molecule was prepared by adding all polar hydrogens with no bond order using a graphical user interface of ADT. The ligands were also prepared as PDB format from all the optimized Gaussian output to assist rigid docking process. Active torsions were set to a maximum number of atoms. Kollman charges have been assigned to the protein and Gasteiger charges to ligands. A pre-calculated grid map was required in ADT for each atom type in the ligand being docked to know the interacting potential energy by preparing grid box so that it covered all the active site of amino acid residues prior to binding. The input grid box have size  $50\times40\times50$  Å (x, y and z)and center at -10.629, 13.455, 113.109(x, y and z) with spacing 0.375 Å using AutoGrid 4.0, integrated in ADT. Lamarckian genetic algorithm (LGA) was kept as default in all separate molecular docking. The best docked models, with higher negative binding energies, were considered for further studies. All docking visualizations were performed using Discovery studio visualizer.

#### Molecular Dynamics (MD) Simulation

MD study using GROMACS 5.1.1 (http://www.gromacs.org/Downloads) was performed with the minimum energy conformers obtained after docking between proteins (PDB ID:4F5S) and two best-designed compound (R36 and R47). Topology of protein was constructed in pdb2gmx using CHARMM36-jul2021 force-field<sup>[14]</sup> and TIP3P solvation model,<sup>[15]</sup> while ligand topology was generated using CHARMM general force field server (CGenFF).<sup>[16,17]</sup> In this study, we used cubic periodic box setting a minimal distance of 1.0 nm between the protein and the edge of the box. All the protein moieties were neutralized by adding adequate number of ions. Using steepest descent algorithm and conjugate gradient protocol, energy minimization was performed until the maximum force of at least 10 kJ mol<sup>-1</sup> nm<sup>-1</sup>.

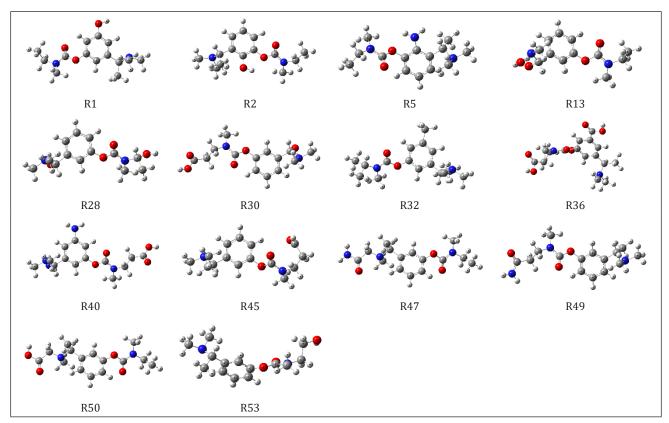


Fig. 2: Best compounds having their G09 optimized structures.

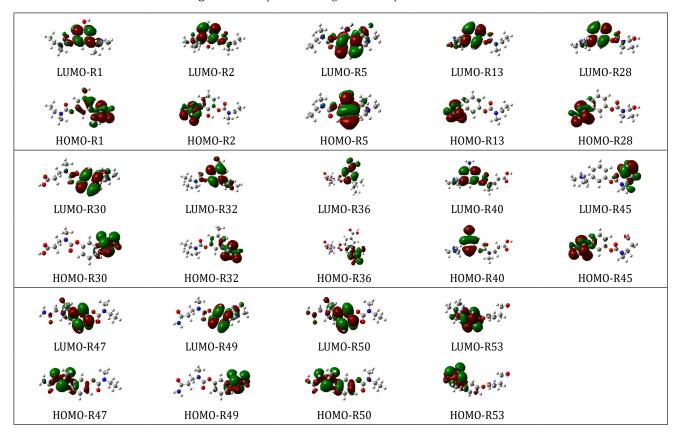


Fig. 3: Contours of the occupied and unoccupied molecular orbitals of the ligands using RB3LYP/6-31G(d,p).



**Table 1:** Compounds having different substituents of rivastigmine and its binding energy.

Compounds	Substituted groups	Substituted by	$\Delta G_{Binding}$ (Kcal/mol)
Rivastigmine	-	-	-6.6
R1	10-H	10-0H	-7.2
R2	11-H	11-0H	-7.0
R3	10-H	10-COOH	-6.7
R4	10-H	10-CONH <sub>2</sub>	-6.8
R5	11-H	11-NH <sub>2</sub>	-6.9
R6	4-CH <sub>3</sub>	4-0H	-7.0
R7	10-Н, 4-СН <sub>3</sub>	10-OH, 4-OH	-6.2
R8	4-CH <sub>3</sub>	4-NO <sub>2</sub>	-7.0
R9	4-CH <sub>3</sub> , 10-H	4-0H, 10-NO <sub>2</sub>	-6.3
R10	10-Н, 4-СН <sub>3</sub>	10-СООН, 4-ОН	-7.0
R11	10-Н, 11-Н	10-OH, 11-CONH <sub>2</sub>	-6.0
R12	10-Н, 11-Н	10-ОН, 11-ОН	-6.3
R13	4-CH <sub>3</sub> , 3-CH <sub>3</sub>	4-0H, 3-0H	-7.0
R14	1-H	1-NH <sub>2</sub>	-6.5
R15	10-H, 4-СН <sub>3</sub> , 17-Н	10-NO <sub>2</sub> , 4-OH, 17-OH	-6.1
R16	2-H, 1-H	2-NH <sub>2</sub> , 1-OH	-6.6
R17	1-H, 2-H	1-0H, 2-0H	-6.6
R18	1-H, 2-H	1-NH <sub>2</sub> , 2-NH <sub>2</sub>	-6.4
R19	13=0	13-0CH <sub>3</sub>	-5.3
R20	10-H	10-0CH <sub>3</sub>	-6.3
R21	10-Н, 11-Н	10-OCH <sub>3</sub> , 11-NH <sub>2</sub>	-6.1
R22	1-H, 2-H, 10-H	1-OH, 2-NH <sub>2</sub> , 10-OH	-6.7
R23	1-H, 10-H, 11-H	1-ОН, 10-ОН, 11-ОН	-6.4
R24	1-H,2-H, 10-H	1-ОН, 2-ОН, 10-ОН	-6.7
R25	8-H, 10-H, 9-H	8-0H, 10-NH <sub>2</sub> , 9-0H	-6.3
R26	10-Н, 11-Н	10-NH <sub>2</sub> ,11-NH <sub>2</sub>	-6.3
R27	10-H, 4-CH <sub>3</sub>	10-СООН, 4-ОН	-6.7
R28	16-H, 4-CH <sub>3</sub>	16-ОН, 4-ОН	-7.1
R29	16-Н, 10-Н	16-ОН, 10-ОН	-6.4
R30	17-H, 4-CH <sub>3</sub>	17-СООН, 4-ОН	-7.1
R31	10-Н, 17-Н	10-CH <sub>3</sub> 17-COOH	-6.4
R32	10-Н, 16-Н	10-CH <sub>3</sub> , 16-CH <sub>3</sub>	-6.7
R33	10-Н, 5-Н	10-СН <sub>2</sub> ОН, 5-ОН	-5.6
R34	10-Н, 17-Н	10-ОН, 17-СООН	-6.5
R35	10-Н, 17-Н	10NO <sub>2</sub> , 17-COOH	-6.0
R36	10-Н, 17-Н	10-СООН, 17-СООН	-7.6
R37	10-Н, 17-Н	10-ОН, 17-СООН	-6.4
R38	10-Н, 17-Н	10-OH, 17-NH <sub>2</sub>	-5.7
R39	10-Н, 17-Н	10-NH <sub>2</sub> , 17-NH <sub>2</sub>	-6.0
R40	10-Н, 17-Н, 4-СН <sub>3</sub>	10-NH <sub>2</sub> ,17-COOH, 4NH <sub>2</sub>	-6.7
R41	10-Н, 17-Н	10-NH <sub>2</sub> , 17NO <sub>2</sub>	-6.5
R42	17-H, 1-H	17-СООН, 1-ОН	-7.0
R43	17-H, 1-H	17-ОН, 1-СООН	-6.5

R44	1-H	1-CHO	-6.6
R45	17-H	17-CHO	-6.9
R46	1-H, 17-H	1-CHO, 17-CHO	-6.3
R47	1-H	1-CONH <sub>2</sub>	-7.5
R48	1-Н, 17-Н	$1\text{-}CONH_2, 17\text{-}CONH_2$	-6.4
R49	17-H	17-CONH <sub>2</sub>	-6.7
R50	1-H	1-COOH	-6.8
R52	1-H	1-F	-6.6
R53	17-H	17-OH	-6.9

Isochoric-isothermal (NVT) and isothermal-isobaric (NPT) ensembles were applied on the system for 100ps for equilibration at 300K by keeping 2-fs time step and 1.2 nm electrostatic and van der Waal cut-offs. Particle mesh Ewald (PME)<sup>[18]</sup> method was used for long range electrostatic interaction calculations. Finally, 10 ns MD simulation was subjected to the equilibrated ensembles with the same cutoffs. Various geometrical properties of the systems such as root mean square deviation (RMSD), root mean square fluctuation (RMSF), solvent-accessible surface area (SASA) and radius of gyration were determined using gmxrmsd, gmxrmsf, gmxsasa and gmx gyrate programs. The graphs were plotted using Origin tool.

# **Binding Free Energy Calculation by MMPBSA**

In this present work, we have determined the molecular mechanics of Poison-Boltzmann surface area (MM/PBSA) free binding energy between the proteins and ligands (R36 and R47) using the g\_mmpbsa tool. [19,20] The MM-PBSA method allows us to estimate the free binding energy of complexation from molecular dynamics trajectories. [21] This method can be used in the application of virtual screens or docking to refine the classification of poses. In this technique,  $\Delta G_{bind}$  is assessed from the free energies of the protein-ligand system in equation 1:

 $\Delta G_{\rm bind} = G_{\rm protein-ligand} - (G_{\rm protein} + G_{\rm ligand})$ The free energy for each individual entity is given by equation 2:

$$G_{ij} = E_{MM} + G_{col} - TS_{MM}$$
 (2)

 $G_x = E_{MM} + G_{solv} - TS_{MM} \qquad (2)$  where, x denotes the protein or ligand or protein–ligand complex,  $E_{MM}$  is the molecular mechanics potential energy in vacuum, and G<sub>solv</sub> is the free energy of solvation. Here, TS denotes to the entropic contribution to the free energy in vacuum, where T and S represent the temperature and entropy, respectively.

The solvation-free energy is the sum of polar and non-polar free energy:

$$G_{\text{solv}} = G_{\text{polar}} + G_{\text{non-polar}}$$
 (3)

Here,  $E_{MM}$  contains the bonded and non-bonded interactions energy which comprise both electrostatic ( $E_{\rm elec}$ ) and van der Waals ( $E_{vdw}$ ) interactions.

$$E_{MM} = E_{non-bonded} + E_{bonded} + (E_{vdw} + E_{elec})$$
 (4)

## RESULTS AND DISCUSSION

It was shown from Table S1, that all the compounds used in this study were successfully qualified the Lipinski's rule of five<sup>[22]</sup> and CMC like rule. Except few of them, most of these ligands were predicted to have good oral bioavailability (Table 3). A large number of compounds have shown excellent permeability, while few have relatively less or poor permeability (Table 4). The derived physical parameters like ionization potential (I), electron affinity (A), global hardness (n), softness (S), chemical potential ( $\mu$ ), electronegativity ( $\sigma$ ), and electrophilicity ( $\omega$ ), play an important role to decide activity of these derived compounds (Table S2). The drug score and drug-likeness values for the ligands were also predicted and are shown in Table S3. It was revealed from the data that 27 compounds have drug score value, in the range of 0.5-0.95, and the rest of the compounds between 0.08-0.49.

Toxicity effect can predict the fate of a promising drug. It has been shown that drug molecules having low toxicity/side effects, contain the high order of the therapeutic index. So toxicity prediction was done for all the derived compounds using OSIRIS property explorer (Table S4). It was noted that all the derived compounds, except few of them have higher or moderate toxicity. The toxicity parameters were used in OSIRIS as color codes, as usual, green stands for low, yellow stands for mediocre, and red stands for high toxicity. The molecular docking results revealed that the docked complex of 23 derived compounds have higher negative binding energies (docked with PDB: 4F5S) compared to standard rivastigmine (-6.6 Kcal/mol) (Table 1).

# **DFT Analysis**

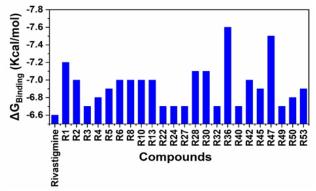
There are several ways, in which chemical stability of a molecule can be calculated. The simplest one involves difference in energy between highest occupied molecular orbital (HOMO) and lowest unoccupied molecular orbitals (LUMO) of a system. It is also a key parameter in determining the molecular properties of a molecule. (22) Energy of HOMO and LUMO are computed theoretically by DFT-RB3LYP/6-31G(d,p) method and the contour diagrams of best molecules are shown in Fig. 3, where positive and negative lobes are noted as red and green color, respectively.



 $\textbf{Table 2:} \ \textbf{Calculated energy values of rivastigmine and its derivatives using rb3lyp/6-31g(d,p)\ basis\ set$ 

Molecule	E <sub>HOMO</sub> (eV)	E <sub>LUMO</sub> (eV)	$\Delta E_{HL}(Band gap)$ (eV)	Energy (eV)×10 <sup>-4</sup>	Dipole Moment (Debye)
Rivastagmine	-5.57	0.09	5.65	-2.20	2.85
R1	-5.64	0.06	5.70	-2.40	2.87
R2	-5.29	0.04	5.33	-2.40	3.62
R3	-6.00	1.26	7.26	-2.71	4.84
R4	-5.84	0.90	6.75	-2.65	3.23
R5	-5.34	0.27	5.61	-2.35	3.87
R6	-6.00	0.04	6.04	-2.29	3.32
R7	-6.00	0.18	6.18	-2.50	1.07
R8	-6.47	1.68	8.15	-2.64	6.20
R9	-6.35	2.14	8.50	-2.85	8.07
R10	-6.08	1.15	7.22	-2.81	3.03
R11	-5.72	0.06	5.77	-2.86	4.61
R12	-5.25	0.07	5.32	-2.60	2.77
R13	-5.82	-0.40	5.42	-2.39	3.68
R14	-5.73	0.13	5.85	-2.35	3.34
R15	-6.27	-2.20	4.07	-3.05	6.26
R16	-5.94	0.09	6.04	-2.55	3.75
R17	-5.90	0.06	5.96	-2.60	4.49
R18	-5.69	0.12	5.81	-2.50	2.05
R19	-5.69	0.12	5.81	-2.31	1.08
R20	-5.65	0.14	5.79	-2.51	2.83
R21	-4.87	0.24	5.11	-2.66	3.45
R22	-5.85	0.03	5.89	-2.76	2.19
R23	-5.30	0.01	5.31	-2.81	3.94
R24	-5.79	0.09	5.89	-2.81	4.36
R25	-5.36	0.29	5.65	-2.76	3.99
R26	-4.64	0.31	4.96	-2.50	2.49
R27	-6.06	-1.17	4.89	-2.81	8.17
R28	-5.96	-0.16	5.80	-2.50	2.3762
R29	-5.80	0.07	5.87	-2.60	2.0027
R30	-6.00	-0.22	5.77	-2.81	1.727
R31	-5.73	0.05	5.78	-2.82	2.5194
R32	-5.70	0.14	5.83	-2.41	2.542
R33	-5.33	0.21	5.53	-2.71	0.7392
R34	-5.83	0.01	5.84	-2.91	2.9496
R35	-6.00	-2.27	3.73	-3.26	8.437
R36	-5.73	-1.25	4.48	-3.22	3.3553
R37	-5.83	0.01	5.84	-2.91	2.9502
R38	-5.71	0.14	5.85	-2.55	2.2473
R39	-5.33	0.23	5.56	-2.50	0.8264
R40	-5.46	0.02	5.49	-2.90	3.8067
R41	-5.53	-1.83	3.70	-2.90	4.2946
R42	-5.94	-0.04	5.89	-2.91	3.2099

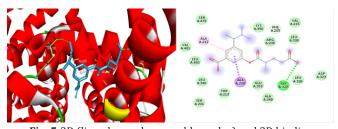
R43	-6.13	-0.14	5.99	-2.91	6.9339
R44	-6.17	-0.69	5.49	-2.50	4.9539
R45	-5.71	-0.64	5.07	-2.50	3.2332
R46	-6.28	-0.86	5.42	-2.81	4.0118
R47	-5.79	0.11	5.90	-2.65	5.5286
R48	-5.82	0.05	5.87	-3.11	3.1368
R49	-5.76	0.04	5.80	-2.65	1.9587
R50	-6.08	-0.03	6.05	-2.71	6.696
R52	-6.22	-0.01	6.20	-2.47	2.204
R53	-5.77	0.02	5.80	-2.40	2.0585



**Fig. 4:** Comparison of binding energies of the best 23 compounds with the receptor (PDB: 4F5S).

HOMO can donate electron and behave as nucleophile; on the other hand, LUMO has electron accepting tendency from nucleophile, behave like electrophile.<sup>[23]</sup>

The chemical reactivity, kinetic stability, optical polarizability and chemical hardness-softness of a molecule depend on the band gap energy ( $\Delta E_{HL}$ ) of HOMO and LUMO. Molecule possessing small  $\Delta E_{HL}$ , has higher chemical reactivity as well as highly polarizable and behaves as soft molecule. [24,25] On the other hand, a relatively higher  $\Delta E_{HL}$  value indicates high chemical stability as well as least chemical reactivity for a molecule. Besides, the molecules with higher dipole moment have a tendency to participate in strong intermolecular interaction. The chemical softness of the molecules depends on the degree of chemical reactivity and the reverse is in the case of hardness. [26]



**Fig. 5:**3D (ligands are shown as blue color) and 2D binding interaction (H- bonds are shown as green lines) of R36 into the binding site of bovine serum albumin with PDB ID: 4F5S.

In this study, we have found 34 derived molecules with higher  $\Delta E_{HL}$  value (>5.65eV) and the remaining 19compounds with low or slightly small  $\Delta E_{HL}$  value (<5.65eV). Among them,R9 has the highest value (8.5eV) and therefore, it is highly unreactive species. On the other hand, R41 is the compound possessing the lowest  $\Delta E_{HL}$  of 3.7eV and is considered as highly polarizable, reactive species i.e. soft compound. From dipole moment parameters, it is found that 7 compounds such as R8, R9, R15, R27, R35, R43 and R50 have larger tendency, to participate in strong intermolecular interaction (dipole moment > 6 Debye).

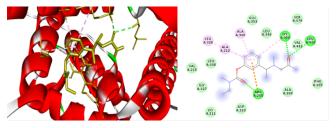
# **Global Reactivity Descriptors**

In order to understand various aspects of pharmacological properties and the eco-toxicological character of drug molecules, several new chemical descriptor parameters have been developed. Conceptual DFT based parameters were used to understand the structure, and reactivity of molecules by calculating various useful parameters like chemical potential, global hardness, softness and electrophilicity index. Using HOMO and LUMO energy, the ionization potential (I) and electron affinity (A) can expressed as

$$I = -E_{HOMO} \tag{1}$$

$$A = -E_{I,IIMO} \tag{2}$$

Using these values, other descriptor properties such as chemical potential ( $\mu$ ), global hardness ( $\eta$ ), global softness (S), electronegativity ( $\sigma$ ) and electrophilicity index ( $\omega$ ) were calculated.



**Fig. 6:**3D (ligands are shown as blue color) and 2D binding interaction (H- bonds are shown as green lines) of R47 into the binding site of bovine serum albumin with PDB ID: 4F5S.



**Table 3:** Pre-admet prediction of rivastigmine and compounds.

Rivastignine         2.28         32.78         18         4         0         0         5         254.01           R1         1.75         53.01         19         5         1         0         5         262.03           R2         1.79         53.01         19         5         1         0         5         262.03           R3         2.14         70.08         21         6         1         0         6         281.01           R4         1.05         75.88         21         6         2         0         6         284.29           R5         1.69         58.80         19         5         2         0         5         265.30           R6         1.25         53.01         18         5         1         0         5         2545.47           R7         0.73         73.24         19         6         2         0         5         253.49           R8         1.67         78.61         20         7         0         0         6         260.81           R10         1.12         90.31         21         7         2         0         6         272.47	Compounds	miLogP	TPSA <sup>a</sup>	Natoms <sup>b</sup>	$nON^c$	nOHNH <sup>d</sup>	n-violations <sup>e</sup>	nrotb <sup>f</sup>	volume
R2         1.79         53.01         19         5         1         0         5         262.03           R3         2.14         70.08         21         6         1         0         6         281.01           R4         1.05         75.88         21         6         2         0         6         281.01           R5         1.69         58.80         19         5         2         0         5         265.30           R6         1.25         53.01         18         5         1         0         5         245.47           R7         0.73         73.24         19         6         2         0         6         260.79           R8         1.67         78.61         20         7         0         0         6         260.79           R9         1.17         98.83         21         8         1         0         6         263.49           R10         1.12         90.31         21         7         2         0         6         272.47           R11         0.50         96.10         22         7         3         0         5         270.05	Rivastigmine	2.28	32.78	18	4	0	0	5	254.01
R3         2.14         70.08         21         6         1         0         6         281.01           R4         1.05         75.88         21         6         2         0         6         284.29           R5         1.69         58.80         19         5         2         0         5         265.30           R6         1.25         53.01         18         5         1         0         5         245.47           R7         0.73         73.24         19         6         2         0         5         253.49           R8         1.67         78.61         20         7         0         0         6         260.79           R9         1.17         98.83         21         7         2         0         6         260.79           R9         1.12         90.31         21         7         2         0         6         272.47           R10         1.12         90.31         21         7         2         0         6         272.30           R11         0.50         96.10         22         7         3         0         5         270.05	R1	1.75	53.01	19	5	1	0	5	262.03
R4         1.05         75.88         21         6         2         0         6         284.29           R5         1.69         58.80         19         5         2         0         5         265.30           R6         1.25         53.01         18         5         1         0         5         245.47           R7         0.73         73.24         19         6         2         0         5         253.49           R8         1.67         78.61         20         7         0         0         6         260.79           R9         1.17         98.83         21         8         1         0         6         268.81           R10         1.12         90.31         21         7         2         0         6         268.81           R11         0.50         96.10         22         7         3         0         6         272.47           R12         1.26         73.24         20         6         2         0         5         270.05           R13         0.94         73.24         18         6         2         0         7         277.00	R2	1.79	53.01	19	5	1	0	5	262.03
R5         1.69         58.80         19         5         2         0         5         265.30           R6         1.25         53.01         18         5         1         0         5         245.47           R7         0.73         73.24         19         6         2         0         5         253.49           R8         1.67         78.61         20         7         0         0         6         260.79           R9         1.17         98.83         21         8         1         0         6         268.81           R10         1.12         90.31         21         7         2         0         6         272.47           R11         0.50         96.10         22         7         3         0         6         272.47           R11         0.50         96.10         22         7         3         0         6         272.47           R11         0.50         96.10         22         7         3         0         6         272.07           R12         1.26         73.24         18         6         2         0         7         277.06	R3	2.14	70.08	21	6	1	0	6	281.01
R6         1.25         53.01         18         5         1         0         5         245.47           R7         0.73         73.24         19         6         2         0         5         253.49           R8         1.67         78.61         20         7         0         0         6         260.79           R9         1.17         98.83         21         7         2         0         6         268.81           R10         1.12         90.31         21         7         2         0         6         272.47           R11         0.50         96.10         22         7         3         0         6         292.30           R12         1.26         73.24         18         6         2         0         5         270.05           R13         0.94         73.24         18         6         2         0         5         236.93           R14         1.67         58.83         20         6         2         0         7         277.06           R15         0.16         119.06         22         9         2         0         7         277.07 <td>R4</td> <td>1.05</td> <td>75.88</td> <td>21</td> <td>6</td> <td>2</td> <td>0</td> <td>6</td> <td>284.29</td>	R4	1.05	75.88	21	6	2	0	6	284.29
R7         0.73         73.24         19         6         2         0         5         253.49           R8         1.67         78.61         20         7         0         0         6         260.79           R9         1.17         98.83         21         8         1         0         6         260.71           R10         1.12         90.31         21         7         2         0         6         272.47           R11         0.50         96.10         22         7         3         0         6         272.47           R12         1.26         73.24         20         6         2         0         5         270.05           R13         0.94         73.24         18         6         2         0         5         236.93           R14         1.67         58.80         19         5         2         0         6         265.54           R15         0.16         119.06         22         9         2         0         7         277.06           R16         1.03         79.03         20         6         2         0         7         277.03 </td <td>R 5</td> <td>1.69</td> <td>58.80</td> <td>19</td> <td>5</td> <td>2</td> <td>0</td> <td>5</td> <td>265.30</td>	R 5	1.69	58.80	19	5	2	0	5	265.30
R8         1.67         78.61         20         7         0         0         6         260.79           R9         1.17         98.83         21         8         1         0         6         268.81           R10         1.12         90.31         21         7         2         0         6         272.47           R11         0.50         96.10         22         7         3         0         6         272.47           R12         1.26         73.24         18         6         2         0         5         270.05           R13         0.94         73.24         18         6         2         0         5         236.93           R14         1.67         58.80         19         5         2         0         6         265.54           R15         0.16         119.06         22         9         2         0         7         277.06           R16         1.03         79.03         20         6         3         0         7         277.05           R17         0.99         73.24         20         6         4         0         7         277.05     <	R6	1.25	53.01	18	5	1	0	5	245.47
R9         1.17         98.83         21         8         1         0         6         268.81           R10         1.12         90.31         21         7         2         0         6         272.47           R11         0.50         96.10         22         7         3         0         6         292.30           R12         1.26         73.24         20         6         2         0         5         270.05           R13         0.94         73.24         18         6         2         0         5         236.93           R14         1.67         58.80         19         5         2         0         6         265.54           R15         0.16         119.06         22         9         2         0         7         277.06           R16         1.03         79.03         20         6         2         0         7         277.07           R16         1.03         79.03         20         6         4         0         7         277.07           R19         2.69         24.94         19         4         0         7         277.40	R7	0.73	73.24	19	6	2	0	5	253.49
R10         1.12         90.31         21         7         2         0         6         272.47           R11         0.50         96.10         22         7         3         0         6         292.30           R12         1.26         73.24         20         6         2         0         5         270.05           R13         0.94         73.24         18         6         2         0         5         236.93           R14         1.67         58.80         19         5         2         0         6         257.06           R15         0.16         119.06         22         9         2         0         7         277.06           R16         1.03         79.03         20         6         3         0         7         277.06           R16         1.03         79.03         20         6         2         0         7         277.06           R16         1.03         79.03         20         6         4         0         7         277.07           R19         2.69         24.94         19         4         0         0         7         277.40	R8	1.67	78.61	20	7	0	0	6	260.79
R11       0.50       96.10       22       7       3       0       6       292.30         R12       1.26       73.24       20       6       2       0       5       270.05         R13       0.94       73.24       18       6       2       0       5       236.93         R14       1.67       58.80       19       5       2       0       6       265.54         R15       0.16       119.06       22       9       2       0       7       277.06         R16       1.03       79.03       20       6       3       0       7       277.05         R17       0.99       73.24       20       6       2       0       7       277.05         R18       1.07       84.83       20       6       4       0       7       277.07         R19       2.69       24.94       19       4       0       0       7       277.40         R20       2.29       42.02       20       5       0       0       6       279.56         R21       1.70       68.04       21       7       4       0       7 <t< td=""><td>R9</td><td>1.17</td><td>98.83</td><td>21</td><td>8</td><td>1</td><td>0</td><td>6</td><td>268.81</td></t<>	R9	1.17	98.83	21	8	1	0	6	268.81
R12         1.26         73.24         20         6         2         0         5         270.05           R13         0.94         73.24         18         6         2         0         5         236.93           R14         1.67         58.80         19         5         2         0         6         265.54           R15         0.16         119.06         22         9         2         0         7         277.06           R16         1.03         79.03         20         6         3         0         7         273.80           R17         0.99         73.24         20         6         2         0         7         277.07           R18         1.07         84.83         20         6         4         0         7         277.07           R19         2.69         24.94         19         4         0         0         7         277.40           R20         2.29         42.02         20         5         0         0         6         279.56           R21         1.70         68.04         21         7         4         0         7         281.82	R10	1.12	90.31	21	7	2	0	6	272.47
R13         0.94         73.24         18         6         2         0         5         236.93           R14         1.67         58.80         19         5         2         0         6         265.54           R15         0.16         119.06         22         9         2         0         7         277.06           R16         1.03         79.03         20         6         3         0         7         273.80           R17         0.99         73.24         20         6         2         0         7         270.53           R18         1.07         84.83         20         6         4         0         7         277.07           R19         2.69         24.94         19         4         0         0         7         277.40           R20         2.29         42.02         20         5         0         0         6         279.56           R21         1.7         4         0         7         281.82           R22         0.50         99.26         21         7         4         0         5         278.55           R23         0.93	R11	0.50	96.10	22	7	3	0	6	292.30
R14         1.67         58.80         19         5         2         0         6         265.54           R15         0.16         119.06         22         9         2         0         7         277.06           R16         1.03         79.03         20         6         3         0         7         273.80           R17         0.99         73.24         20         6         2         0         7         277.07           R18         1.07         84.83         20         6         4         0         7         277.07           R19         2.69         24.94         19         4         0         0         7         277.40           R20         2.29         42.02         20         5         0         0         6         279.56           R21         1.70         68.04         21         6         2         0         6         290.85           R22         0.50         99.26         21         7         4         0         7         281.82           R23         0.62         93.47         21         7         3         0         6         278.55	R12	1.26	73.24	20	6	2	0	5	270.05
R15         0.16         119.06         22         9         2         0         7         277.06           R16         1.03         79.03         20         6         3         0         7         273.80           R17         0.99         73.24         20         6         2         0         7         277.07           R18         1.07         84.83         20         6         4         0         7         277.07           R19         2.69         24.94         19         4         0         0         7         277.40           R20         2.29         42.02         20         5         0         0         6         279.56           R21         1.70         68.04         21         6         2         0         6         290.85           R22         0.50         99.26         21         7         4         0         7         281.82           R23         0.62         93.47         21         7         3         0         6         278.31           R24         0.46         93.47         21         7         4         0         5         281.34	R13	0.94	73.24	18	6	2	0	5	236.93
R16         1.03         79.03         20         6         3         0         7         273.80           R17         0.99         73.24         20         6         2         0         7         270.53           R18         1.07         84.83         20         6         4         0         7         277.07           R19         2.69         24.94         19         4         0         0         7         277.40           R20         2.29         42.02         20         5         0         0         6         279.56           R21         1.70         68.04         21         6         2         0         6         290.85           R22         0.50         99.26         21         7         4         0         7         281.82           R23         0.62         93.47         21         7         3         0         6         278.31           R24         0.46         93.47         21         7         4         0         5         281.34           R25         0.93         99.26         21         7         4         0         5         276.59	R14	1.67	58.80	19	5	2	0	6	265.54
R17         0.99         73.24         20         6         2         0         7         270.53           R18         1.07         84.83         20         6         4         0         7         277.07           R19         2.69         24.94         19         4         0         0         7         277.40           R20         2.29         42.02         20         5         0         0         6         279.56           R21         1.70         68.04         21         6         2         0         6         290.85           R22         0.50         99.26         21         7         4         0         7         281.82           R23         0.62         93.47         21         7         3         0         6         278.31           R24         0.46         93.47         21         7         3         0         7         278.55           R25         0.93         99.26         21         7         4         0         5         281.34           R26         0.71         84.83         20         6         4         0         5         276.59	R15	0.16	119.06	22	9	2	0	7	277.06
R18       1.07       84.83       20       6       4       0       7       277.07         R19       2.69       24.94       19       4       0       0       7       277.40         R20       2.29       42.02       20       5       0       0       6       279.56         R21       1.70       68.04       21       6       2       0       6       279.55         R22       0.50       99.26       21       7       4       0       7       281.82         R23       0.62       93.47       21       7       3       0       6       278.31         R24       0.46       93.47       21       7       3       0       7       278.55         R25       0.93       99.26       21       7       4       0       5       281.34         R26       0.71       84.83       20       6       4       0       5       276.59         R27       1.12       90.31       21       7       2       0       5       253.51         R28       0.60       73.24       19       6       2       0       7 <th< td=""><td>R16</td><td>1.03</td><td>79.03</td><td>20</td><td>6</td><td>3</td><td>0</td><td>7</td><td>273.80</td></th<>	R16	1.03	79.03	20	6	3	0	7	273.80
R19       2.69       24.94       19       4       0       0       7       277.40         R20       2.29       42.02       20       5       0       0       6       279.56         R21       1.70       68.04       21       6       2       0       6       290.85         R22       0.50       99.26       21       7       4       0       7       281.82         R23       0.62       93.47       21       7       3       0       6       278.31         R24       0.46       93.47       21       7       3       0       7       278.55         R25       0.93       99.26       21       7       4       0       5       281.34         R26       0.71       84.83       20       6       4       0       5       276.59         R27       1.12       90.31       21       7       2       0       6       272.47         R28       0.60       73.24       19       6       2       0       5       253.51         R29       1.09       73.24       20       6       2       0       7 <th< td=""><td>R17</td><td>0.99</td><td>73.24</td><td>20</td><td>6</td><td>2</td><td>0</td><td>7</td><td>270.53</td></th<>	R17	0.99	73.24	20	6	2	0	7	270.53
R20       2.29       42.02       20       5       0       0       6       279.56         R21       1.70       68.04       21       6       2       0       6       290.85         R22       0.50       99.26       21       7       4       0       7       281.82         R23       0.62       93.47       21       7       3       0       6       278.31         R24       0.46       93.47       21       7       3       0       7       278.55         R25       0.93       99.26       21       7       4       0       5       281.34         R26       0.71       84.83       20       6       4       0       5       276.59         R27       1.12       90.31       21       7       2       0       6       272.47         R28       0.60       73.24       19       6       2       0       5       253.51         R29       1.09       73.24       20       6       2       0       7       272.71         R31       1.82       70.08       22       6       1       0       7 <th< td=""><td>R18</td><td>1.07</td><td>84.83</td><td>20</td><td>6</td><td>4</td><td>0</td><td>7</td><td>277.07</td></th<>	R18	1.07	84.83	20	6	4	0	7	277.07
R21       1.70       68.04       21       6       2       0       6       290.85         R22       0.50       99.26       21       7       4       0       7       281.82         R23       0.62       93.47       21       7       3       0       6       278.31         R24       0.46       93.47       21       7       3       0       7       278.55         R25       0.93       99.26       21       7       4       0       5       281.34         R26       0.71       84.83       20       6       4       0       5       276.59         R27       1.12       90.31       21       7       2       0       6       272.47         R28       0.60       73.24       19       6       2       0       5       253.51         R29       1.09       73.24       20       6       2       0       7       272.71         R31       1.82       70.08       22       6       1       0       7       297.82         R33       0.56       73.24       21       6       2       0       7 <th< td=""><td>R19</td><td>2.69</td><td>24.94</td><td>19</td><td>4</td><td>0</td><td>0</td><td>7</td><td>277.40</td></th<>	R19	2.69	24.94	19	4	0	0	7	277.40
R22       0.50       99.26       21       7       4       0       7       281.82         R23       0.62       93.47       21       7       3       0       6       278.31         R24       0.46       93.47       21       7       3       0       7       278.55         R25       0.93       99.26       21       7       4       0       5       281.34         R26       0.71       84.83       20       6       4       0       5       276.59         R27       1.12       90.31       21       7       2       0       6       272.47         R28       0.60       73.24       19       6       2       0       5       253.51         R29       1.09       73.24       20       6       2       0       5       270.80         R30       0.40       90.31       21       7       2       0       7       297.82         R32       2.97       32.78       20       4       0       0       5       287.16         R33       0.56       73.24       21       6       2       0       7 <td< td=""><td>R20</td><td>2.29</td><td>42.02</td><td>20</td><td>5</td><td>0</td><td>0</td><td>6</td><td>279.56</td></td<>	R20	2.29	42.02	20	5	0	0	6	279.56
R23       0.62       93.47       21       7       3       0       6       278.31         R24       0.46       93.47       21       7       3       0       7       278.55         R25       0.93       99.26       21       7       4       0       5       281.34         R26       0.71       84.83       20       6       4       0       5       276.59         R27       1.12       90.31       21       7       2       0       6       272.47         R28       0.60       73.24       19       6       2       0       5       253.51         R29       1.09       73.24       20       6       2       0       5       270.80         R30       0.40       90.31       21       7       2       0       7       272.71         R31       1.82       70.08       22       6       1       0       7       297.82         R32       2.97       32.78       20       4       0       0       5       287.16         R33       0.56       73.24       21       6       2       0       7 <td< td=""><td>R21</td><td>1.70</td><td>68.04</td><td>21</td><td>6</td><td>2</td><td>0</td><td>6</td><td>290.85</td></td<>	R21	1.70	68.04	21	6	2	0	6	290.85
R24       0.46       93.47       21       7       3       0       7       278.55         R25       0.93       99.26       21       7       4       0       5       281.34         R26       0.71       84.83       20       6       4       0       5       276.59         R27       1.12       90.31       21       7       2       0       6       272.47         R28       0.60       73.24       19       6       2       0       5       253.51         R29       1.09       73.24       20       6       2       0       5       270.80         R30       0.40       90.31       21       7       2       0       7       272.71         R31       1.82       70.08       22       6       1       0       7       297.82         R32       2.97       32.78       20       4       0       0       5       287.16         R33       0.56       73.24       21       6       2       0       7       289.27         R34       0.89       90.31       22       7       2       0       7 <td< td=""><td>R22</td><td>0.50</td><td>99.26</td><td>21</td><td>7</td><td>4</td><td>0</td><td>7</td><td>281.82</td></td<>	R22	0.50	99.26	21	7	4	0	7	281.82
R25       0.93       99.26       21       7       4       0       5       281.34         R26       0.71       84.83       20       6       4       0       5       276.59         R27       1.12       90.31       21       7       2       0       6       272.47         R28       0.60       73.24       19       6       2       0       5       253.51         R29       1.09       73.24       20       6       2       0       5       270.80         R30       0.40       90.31       21       7       2       0       7       272.71         R31       1.82       70.08       22       6       1       0       7       297.82         R32       2.97       32.78       20       4       0       0       5       287.16         R33       0.56       73.24       21       6       2       0       7       287.09         R34       0.89       90.31       22       7       2       0       7       289.27         R35       1.33       115.90       24       9       1       0       8 <t< td=""><td>R23</td><td>0.62</td><td>93.47</td><td>21</td><td>7</td><td>3</td><td>0</td><td>6</td><td>278.31</td></t<>	R23	0.62	93.47	21	7	3	0	6	278.31
R26       0.71       84.83       20       6       4       0       5       276.59         R27       1.12       90.31       21       7       2       0       6       272.47         R28       0.60       73.24       19       6       2       0       5       253.51         R29       1.09       73.24       20       6       2       0       5       270.80         R30       0.40       90.31       21       7       2       0       7       272.71         R31       1.82       70.08       22       6       1       0       7       297.82         R32       2.97       32.78       20       4       0       0       5       287.16         R33       0.56       73.24       21       6       2       0       7       287.09         R34       0.89       90.31       22       7       2       0       7       289.27         R35       1.33       115.90       24       9       1       0       8       304.59         R36       1.28       107.38       24       8       2       0       8       <	R24	0.46	93.47	21	7	3	0	7	278.55
R27       1.12       90.31       21       7       2       0       6       272.47         R28       0.60       73.24       19       6       2       0       5       253.51         R29       1.09       73.24       20       6       2       0       5       270.80         R30       0.40       90.31       21       7       2       0       7       272.71         R31       1.82       70.08       22       6       1       0       7       297.82         R32       2.97       32.78       20       4       0       0       5       287.16         R33       0.56       73.24       21       6       2       0       7       287.09         R34       0.89       90.31       22       7       2       0       7       289.27         R35       1.33       115.90       24       9       1       0       8       304.59         R36       1.28       107.38       24       8       2       0       8       308.26	R25	0.93	99.26	21	7	4	0	5	281.34
R28       0.60       73.24       19       6       2       0       5       253.51         R29       1.09       73.24       20       6       2       0       5       270.80         R30       0.40       90.31       21       7       2       0       7       272.71         R31       1.82       70.08       22       6       1       0       7       297.82         R32       2.97       32.78       20       4       0       0       5       287.16         R33       0.56       73.24       21       6       2       0       7       287.09         R34       0.89       90.31       22       7       2       0       7       289.27         R35       1.33       115.90       24       9       1       0       8       304.59         R36       1.28       107.38       24       8       2       0       8       308.26	R26	0.71	84.83	20	6	4	0	5	276.59
R29       1.09       73.24       20       6       2       0       5       270.80         R30       0.40       90.31       21       7       2       0       7       272.71         R31       1.82       70.08       22       6       1       0       7       297.82         R32       2.97       32.78       20       4       0       0       5       287.16         R33       0.56       73.24       21       6       2       0       7       287.09         R34       0.89       90.31       22       7       2       0       7       289.27         R35       1.33       115.90       24       9       1       0       8       304.59         R36       1.28       107.38       24       8       2       0       8       308.26	R27	1.12	90.31	21	7	2	0	6	272.47
R30       0.40       90.31       21       7       2       0       7       272.71         R31       1.82       70.08       22       6       1       0       7       297.82         R32       2.97       32.78       20       4       0       0       5       287.16         R33       0.56       73.24       21       6       2       0       7       287.09         R34       0.89       90.31       22       7       2       0       7       289.27         R35       1.33       115.90       24       9       1       0       8       304.59         R36       1.28       107.38       24       8       2       0       8       308.26	R28	0.60	73.24	19	6	2	0	5	253.51
R31       1.82       70.08       22       6       1       0       7       297.82         R32       2.97       32.78       20       4       0       0       5       287.16         R33       0.56       73.24       21       6       2       0       7       287.09         R34       0.89       90.31       22       7       2       0       7       289.27         R35       1.33       115.90       24       9       1       0       8       304.59         R36       1.28       107.38       24       8       2       0       8       308.26	R29	1.09	73.24	20	6	2	0	5	270.80
R32       2.97       32.78       20       4       0       0       5       287.16         R33       0.56       73.24       21       6       2       0       7       287.09         R34       0.89       90.31       22       7       2       0       7       289.27         R35       1.33       115.90       24       9       1       0       8       304.59         R36       1.28       107.38       24       8       2       0       8       308.26	R30	0.40	90.31	21	7	2	0	7	272.71
R33       0.56       73.24       21       6       2       0       7       287.09         R34       0.89       90.31       22       7       2       0       7       289.27         R35       1.33       115.90       24       9       1       0       8       304.59         R36       1.28       107.38       24       8       2       0       8       308.26	R31	1.82	70.08	22	6	1	0	7	297.82
R34     0.89     90.31     22     7     2     0     7     289.27       R35     1.33     115.90     24     9     1     0     8     304.59       R36     1.28     107.38     24     8     2     0     8     308.26	R32	2.97	32.78	20	4	0	0	5	287.16
R35 1.33 115.90 24 9 1 0 8 304.59 R36 1.28 107.38 24 8 2 0 8 308.26	R33	0.56	73.24	21	6	2	0	7	287.09
R36 1.28 107.38 24 8 2 0 8 308.26	R34	0.89	90.31	22	7	2	0	7	289.27
	R35	1.33	115.90	24	9	1	0	8	304.59
R37 0.89 90.31 22 7 2 0 7 289.27	R36	1.28	107.38	24	8	2	0	8	308.26
	R37	0.89	90.31	22	7	2	0	7	289.27
R38 0.18 79.03 20 6 3 0 6 273.56	R38	0.18	79.03	20	6	3	0	6	273.56
R39 -0.27 84.83 20 6 4 0 6 276.83	R39	-0.27	84.83	20	6	4	0	6	276.83
R40 -0.53 122.13 22 8 5 0 7 287.27	R40	-0.53	122.13	22	8	5	0	7	287.27
R41 0.71 104.63 22 8 2 0 7 288.88	R41	0.71	104.63	22	8	2	0	7	288.88
R42 0.77 90.31 22 7 2 0 8 289.51	R42	0.77	90.31	22	7	2	0	8	289.51

R43	-40	90.31	22	7	2	0	8	289.51
R44	2.10	49.85	20	5	0	0	7	273.24
R45	1.99	49.85	20	5	0	0	7	273.24
R46	1.81	66.92	22	6	0	0	9	292.46
R47	1.01	75.88	21	6	2	0	7	284.53
R48	-0.37	118.97	24	8	4	0	9	315.04
R49	0.90	75.88	21	6	2	0	7	284.53
R50	0.61	70.08	21	6	1	0	7	281.26
R52	2.56	32.78	19	4	0	0	6	259.19
R53	1.27	53.01	19	5	1	0	6	262.27

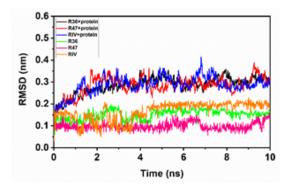
<sup>&</sup>lt;sup>a</sup>Total polar surface area, <sup>b</sup> Number of heavy atoms present in the compound, <sup>c</sup>Number of hydrogen bond acceptors, <sup>d</sup>Number of hydrogen bond donors, <sup>e</sup>Number of violations made by proposed drug, <sup>f</sup>Number of rotatable bonds.

**Table 4:** Molecular descriptor properties of rivastigmine and compounds

Table 4: Molecular descriptor properties of rivastigmine and compounds									
Compounds	BBB	CaCO2	HIA	MDCK	PPB	Skin permeability	SKlogP value	SKlogS pure	
Rivastigmine	1.16217	47.5911	99.415222	43.566	26.387634	-1.968	2.620070	-1.800070	
R1	0.499828	27.361	95.119652	47.5221	34.060016	-2.5506	2.273920	-1.319270	
R2	0.507105	29.2917	95.115064	62.7858	33.642588	-2.59927	2.539070	-1.076470	
R3	1.16082	19.9862	96.066886	42.0786	26.083634	-2.88804	2.592610	-1.790450	
R4	0.666831	19.4172	95.385400	27.9297	18.646095	-3.25799	1.728410	-1.932350	
R5	0.669878	21.96	96.195048	43.743	23.243336	-2.72291	1.825690	-1.528760	
R6	0.495142	19.2016	95.111338	70.6454	12.421550	-2.51509	1.792560	-1.361780	
R7	0.437329	10.2587	90.104534	60.51	16.408142	-3.23631	1.446410	-0.880980	
R8	0.522462	21.9088	92.270924	42.9023	25.620331	-2.97609	2.382270	-2.256620	
R9	0.501965	1.49523	80.855977	59.0592	19.155872	-3.25437	1.877420	-2.007030	
R10	0.437649	15.9586	87.226666	37.3769	15.569182	-3.43019	1.765100	-1.352160	
R11	0.438217	16.4177	88.655356	14.3511	28.479049	-3.63106	1.112830	-1.227450	
R12	0.616661	16.5458	90.651850	42.7282	37.625648	-3.21151	2.192920	-0.595670	
R13	0.103843	20.8027	89.368589	26.6141	41.022845	-3.20828	0.530620	-1.342440	
R14	0.0175174	21.5801	96.324029	45.3978	17.225652	-2.67788	2.066780	-2.567500	
R15	0.216284	1.0979	60.525925	10.4341	17.358162	-3.51279	0.967660	-1.486850	
R16	0.023832	20.4741	91.905337	26.0719	13.886587	-3.42818	1.188110	-1.989880	
R17	0.0676393	20.7256	91.061282	35.2926	15.675083	-3.33625	0.862730	-0.644830	
R18	0.0115219	19.8136	91.885510	16.8589	9.310493	-3.46535	1.513490	-2.807300	
R19	0.829462	56.2171	100.00000	17.1875	11.821660	-1.82551	2.770300	-0.652860	
R20	1.54009	53.0033	98.212480	42.5929	40.593344	-2.37801	2.654010	-1.963580	
R21	0.751316	25.7969	96.221207	33.4496	33.039835	-3.21072	1.859630	-1.692270	
R22	0.0389897	18.9313	81.985830	11.9988	14.092063	-3.83406	0.841960	-1.509080	
R23	0.092552	17.6572	81.250329	19.9822	24.712115	-3.82289	1.314250	-0.018050	
R24	0.0666676	19.6561	81.496460	20.134	15.205758	-3.85747	0.516580	-0.164030	
R25	0.348447	11.0529	82.438500	11.845	28.047205	-3.82667	1.801770	-0.304140	
R26	0.391698	17.8026	92.716853	11.6194	22.260921	-3.44883	1.201830	-1.461090	
R27	0.437649	15.9586	87.226666	37.3769	15.569182	-3.43019	1.765100	-1.352160	
R28	0.0492421	13.7065	90.294917	36.9091	13.047045	-3.34158	1.193290	-1.059190	
R29	0.0858579	20.8544	90.860353	32.6935	29.966602	-3.33997	1.674650	-1.016680	
R30	0.0103935	16.7608	87.226666	69.3047	14.297849	-3.30426	1.254540	-0.916790	
R31	0.0147745	21.0226	96.724100	5.54605	33.951423	-2.88478	2.646100	-1.859310	



R32	0.820849	50.427	99.263889	28.2848	41.023275	-1.91623	3.555460	-2.528110
R33	0.0572076	21.5686	91.695589	7.05786	15.973843	-3.55755	1.265000	-1.138680
R34	0.0196515	17.419	88.868483	29.4785	30.463008	-3.31133	1.735900	-0.874280
R35	0.0136545	6.80734	73.290720	1.34827	31.172896	-3.08256	2.166910	-2.000330
R36	0.0102649	18.9216	82.599427	2.00461	25.521346	-3.39524	2.054590	-1.859410
R37	0.0196515	17.419	88.868483	29.4785	30.463008	-3.31133	1.735900	-0.874280
R38	0.0282392	15.7963	91.516824	16.307	9.886880	-3.47194	1.273200	-1.206700
R39	0.0265201	17.8075	92.198461	5.69546	8.974546	-3.55301	0.995290	-1.619830
R40	0.033625	16.677	70.475794	38.0002	9.874006	-3.75078	0.539520	-1.784360
R41	0.0100495	4.89886	83.352323	19.9618	31.814022	-3.25208	1.675960	-2.107060
R42	0.0119574	20.0217	88.920167	37.7191	21.333873	-3.25866	1.203380	-0.777460
R43	0.246817	20.9853	88.922998	14.9907	32.491560	-3.34696	1.455460	-1.174340
R44	1.3459	33.3222	98.177825	68.7048	35.822287	-2.80881	2.065860	-1.855320
R45	0.0197157	29.4287	98.177825	33.4097	24.958010	-2.65353	1.782690	-1.515880
R46	0.197904	24.0667	97.828588	19.136	30.396077	-3.08897	1.228480	-1.571130
R47	0.108342	21.9242	95.376772	22.9231	28.468806	-3.22977	1.501020	-1.836420
R48	0.0296498	20.4505	82.663091	16.5803	13.656903	-3.50769	0.098800	-1.533330
R49	0.0111783	19.677	95.376894	38.8877	19.200908	-3.1864	1.217850	-1.496980
R50	0.922122	22.3153	96.066886	43.4705	39.656796	-3.054	2.365220	-1.694520
R52	0.0749711	31.5965	99.409326	34.7564	27.195640	-2.43243	3.007740	-2.385980
R53	0.0647141	23.3141	95.302478	42.2241	27.981614	-2.77693	1.710310	-1.279890



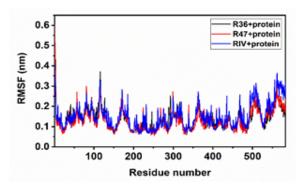


Fig. 7: (a) RMSD plot of protein-ligand complexes with the receptor, (b) RMSF of all amino acids of the protein, complexes with their ligands.

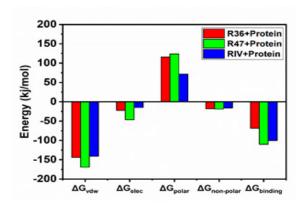


Fig. 8: Different types of energies of docked ligandswith the protein.

$$\mu = \frac{ELUMO + EHOMO}{2}$$

$$\eta = \frac{E_{LUMO} - E_{HOMO}}{2}$$

$$S = \frac{1}{\eta}$$

$$\sigma = -\mu$$
(3)
(4)
(5)

$$\omega = \frac{\mu^2}{2} \tag{7}$$

Chemical stability of a system is represented by global hardness. [24] This property predicts the measure of resistance to change the distribution of electronic charge in a molecule. [25] According to Parr, electrophilicity index ( $\omega$ ) determines a species's capacity to accept electron. [26] The lower chemical hardness value ( $\eta \le 2.83 \, \text{eV}$ ) with low chemical potential ( $\mu < 2.74 \, \text{eV}$ ) of R13, R15, R27, R35, R36,